

Linearized Theory: Sound Waves

In the linearized limit, $\Lambda_{i\alpha}$ becomes $\delta_{i\alpha}$, and the distinction between the reference and target spaces effectively vanishes.

$$u_{\alpha\beta} \rightarrow (\partial_i u_j + \partial_j u_i) / 2 \quad u_i(\mathbf{x}) \sim e^{i\mathbf{q}\cdot\mathbf{x}} = e^{i(q_x x + q_y y)}$$

$$F = \frac{1}{2} \int \frac{d^D q}{(2\pi)^D} u_i(-\mathbf{q}) K_{ij}(\mathbf{q}) u_j(\mathbf{q}) \quad K_{ij}(q) = \mu q^2 \delta_{ij}^T + (\lambda + 2\mu) q^2 \hat{q}_i \hat{q}_j$$

$$\rho \ddot{u}_i = f_i = \partial_j \sigma_{ij} = (\lambda + \mu) \partial_i \partial_j u_j + \mu \nabla^2 u_i$$

$$\rho \omega^2 u_i = (\lambda + 2\mu) q_i q_j u_j + \mu q^2 \delta_{ij}^T u_j = K_{ij}(\mathbf{q}) u_j$$

$K_{ij}(\mathbf{q})$:
Rigidity matrix

q_i : wavenumber

$$\delta_{ij}^T = \delta_{ij} - \hat{q}_i \hat{q}_j$$

$$u_{Li} = \hat{q}_i u_L : u_L = \hat{q}_i u_i$$

$$u_{Ti} = \delta_{ij}^T u_j$$

$$\omega_L^2 = c_L^2 q^2; \quad \omega_T^2 = c_T^2 q^2$$

$$c_L^2 = (\lambda + 2\mu) / \rho$$

$$= [B + 2(D - 1)(\mu / D)] / \rho$$

$$c_T^2 = \mu / \rho$$

Note $c_L = c_T$ in 2D when $B=0$

Dynamical matrix and Waves in 2D

$$D_{ij}(\mathbf{q}) = \frac{1}{\rho} K_{ij}(\mathbf{q}) = \frac{1}{\rho} \begin{pmatrix} (\lambda + 2\mu)q_x^2 + \mu q_y^2 & (\lambda + \mu)q_x q_y \\ (\lambda + 2\mu)q_x q_y & (\lambda + 2\mu)q_y^2 + \mu q_x^2 \end{pmatrix}$$

D_{ij} : Continuum dynamical matrix $\omega^2 u_i = D_{ij} u_j$

$$\omega_L^2 = c_L^2 q^2 : \quad u_L = (\hat{q}_x, \hat{q}_y); \quad \hat{\mathbf{q}} = \mathbf{q} / q$$

$$\omega_T^2 = c_T^2 q^2 : \quad u_T = (\hat{q}_y, -\hat{q}_x)$$

2D uniaxial system

$$f = \frac{1}{2} \left(K_1 u_{xx}^2 + 2K_2 u_{xx} u_{yy} + K_3 u_{yy}^2 + 2K_5 u_{xy}^2 \right)$$

$$D_{ij}(\mathbf{q}) = \frac{1}{\rho} \begin{pmatrix} K_1 q_x^2 + K_5 q_y^2 & (K_2 + K_5) q_x q_y \\ (K_2 + K_5) q_x q_y & K_3 q_y^2 + K_5 q_x^2 \end{pmatrix}$$

Surface (Rayleigh) waves

$$\sigma_{yy} = (\lambda + 2\mu)u_{yy} + \lambda u_{xx} \quad u_i(x, y) \propto A e^{iqx - \kappa y} \quad \text{Convert } q_y \text{ to } i\kappa$$

$$\sigma_{xy} = 2\mu u_{xy} \quad q_x^2 + q_y^2 \rightarrow q^2 - \kappa^2$$

$$u_x(x, y) = e^{iqx} \left(qA_L e^{-\kappa_L y} - i\kappa_T A_T e^{-\kappa_T y} \right) \quad \kappa_L^2 = q^2 - (\omega^2 / c_L^2) > 0$$

$$u_y(x, y) = e^{iqx} \left(i\kappa_L A_L e^{-\kappa_L y} + qA_T e^{-\kappa_T y} \right) \quad \kappa_T^2 = q^2 - (\omega^2 / c_T^2) > 0$$

$$\sigma_{yy}(y=0) = e^{iqx} [i(c_L^2(q^2 - \kappa_L^2) - 2q^2 c_T^2)A_L - 2c_T^2 q \kappa_T A_T] = 0$$

$$\sigma_{xy}(y=0) = \mu e^{iqx} [-2q\kappa_L A_L + i(q^2 + \kappa_T^2)A_T] = 0$$

$$\begin{bmatrix} -2q\kappa_L & i(q^2 + \kappa_T^2) \\ i(c_L^2(q^2 - \kappa_L^2) - 2q^2 c_T^2) & -2c_T^2 q \kappa_T \end{bmatrix} \begin{bmatrix} A_L \\ A_T \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \end{bmatrix}$$

$$4q^2 c_T^2 \kappa_T \kappa_L + (q^2 + \kappa_T^2)[c_L^2(q^2 - \kappa_L^2) - 2q^2 c_T^2] = 0$$

Rayleigh Wave Speed

$$[2q^2 - (\omega^2 / c_T^2)][\omega^2 - 2c_T^2 q^2] = 4q^2 \sqrt{[q^2 - (\omega^2 / c_L^2)][q^2 - (\omega^2 / c_T^2)]}$$

$$\omega^2 = c_T^2 s^2 q^2$$

$$s^6 - 8s^4 + 8s^2[3 - 2(c_T^2 / c_L^2)] - 16[1 - (c_T^2 / c_L^2)] = 0$$

Solve subject to the constraint that s^2 , κ_L^2 , and κ_T^2 be greater than zero: only one solution.

$$c_T = c_L \quad s^6 - 8s^4 + 8s^2 = 0$$

Solutions: $s = 0$; $s^2 = 4(1 \pm \sqrt{1/2}) > 1$

Only first soln satisfies constraints.

Response and Fluctuations

$$f_i^{\text{int}}(\mathbf{x}) = -\frac{\delta \mathcal{F}}{\delta u_i(\mathbf{x})} = -\int d^D x' K_{ij}(\mathbf{x}, \mathbf{x}') u_j(\mathbf{x}') = -f_i^{\text{ext}}(\mathbf{x})$$

$$\chi_{ij}(\mathbf{x}, \mathbf{x}') = \frac{\delta u_i(\mathbf{x})}{\delta f_j(\mathbf{x}')} = K_{ij}^{-1}(\mathbf{x}, \mathbf{x}')$$

Note: χ diverges when any eigenmode frequency vanishes

$$\chi_{ij}(\mathbf{q}) = K_{ij}^{-1}(\mathbf{q}) = \frac{\hat{q}_i \hat{q}_j}{(\lambda + 2\mu)q^2} + \frac{\delta_{ij} - \hat{q}_i \hat{q}_j}{\mu q^2}$$

$$S_{ij}(\mathbf{x}, \mathbf{x}') = \langle u_i(\mathbf{x}) u_j(\mathbf{x}') \rangle - \langle u_i(\mathbf{x}) \rangle \langle u_j(\mathbf{x}') \rangle = T \chi_{ij}(\mathbf{x}, \mathbf{x}')$$

$$S_{ij}(\mathbf{q}) = T \chi_{ij}(\mathbf{q}) : \langle \mathbf{u}^2(\mathbf{x}) \rangle \approx \int \frac{d^D q}{(2\pi)^D} \frac{T}{K q^2} \xrightarrow{D \leq 2} \infty$$

$$\langle \rho(\mathbf{x}) \rangle = \sum_{\mathbf{G}} \langle e^{i\mathbf{G} \cdot (\mathbf{x} - \mathbf{u}(\mathbf{x}))} \rangle \rho_{\mathbf{G}}(\mathbf{x}); \quad \langle e^{-i\mathbf{G} \cdot \mathbf{u}(\mathbf{x})} \rangle \approx e^{-G_i \langle u_i u_j \rangle G_j / 2}$$

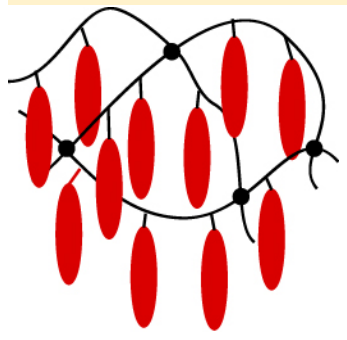
No Long-Range Crystalline Order for $D \leq 2$

What are Nematic Gels?

- Homogeneous Elastic media with broken rotational symmetry (uniaxial, biaxial)
- Most interesting - systems with broken symmetry that develop spontaneously from a homogeneous, isotropic elastic state

Examples of LC Gels

1. Liquid Crystal Elastomers - Weakly crosslinked liquid crystal polymers



Nematic



Smectic-C

2. Tanaka gels with hard-rod dispersion

3. Anisotropic membranes

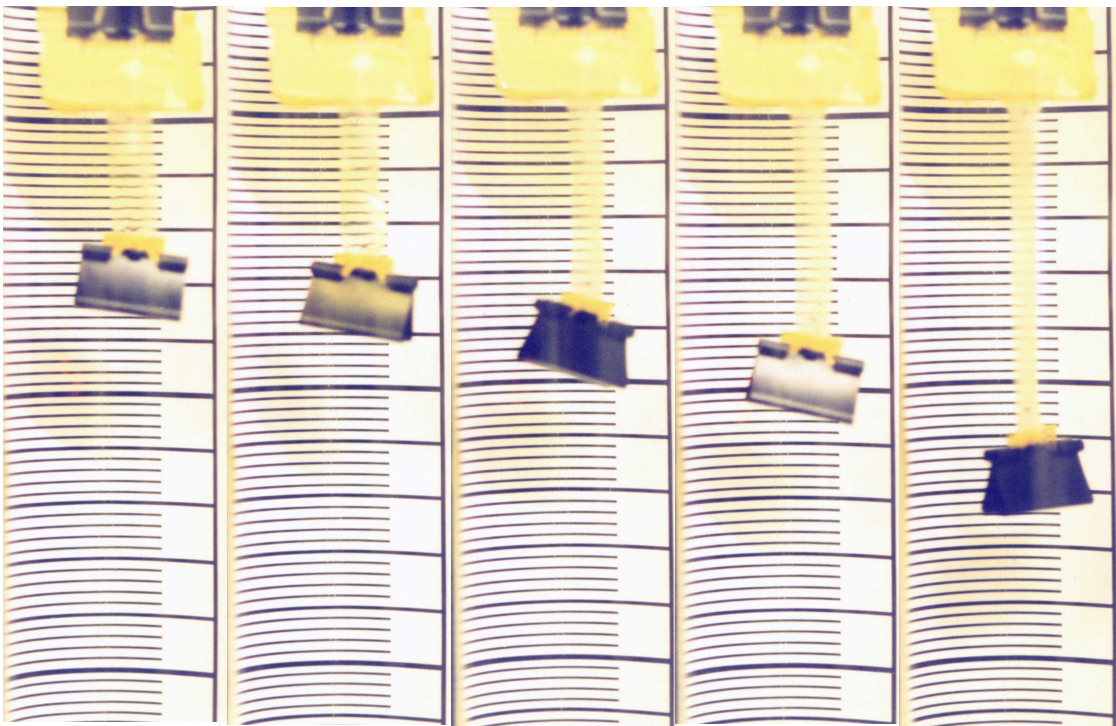


4. Glasses with orientational order



Properties I

- **Large thermoelastic effects** - Large thermally induced strains - artificial muscles

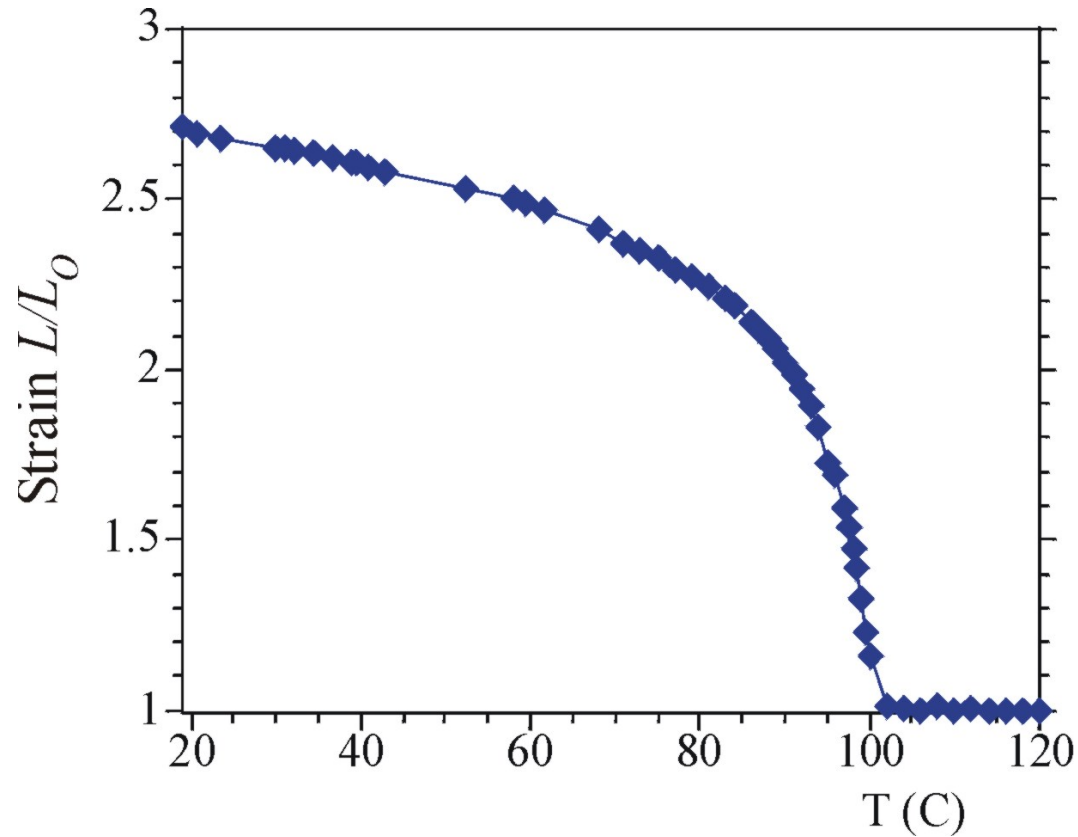


Courtesy of
Eugene Terentjev

300% strain

Properties II

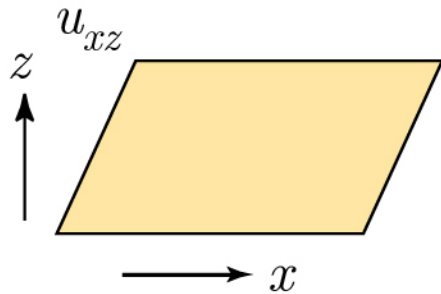
Large strain in small temperature range



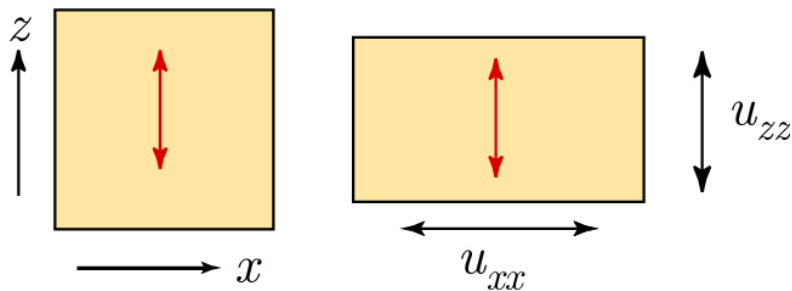
Terentjev

Properties III

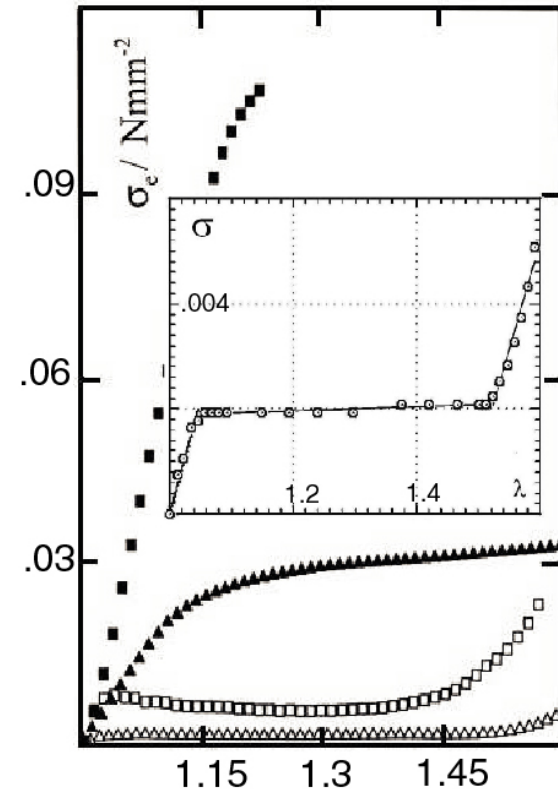
- Soft or “Semi-soft” elasticity



Vanishing xz shear modulus

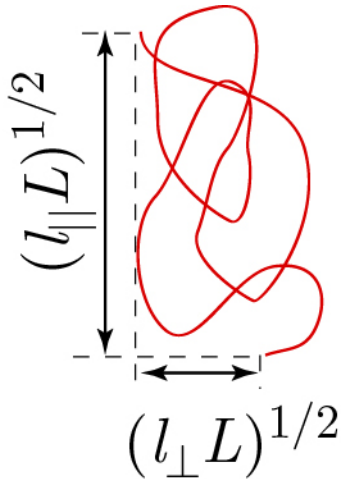


Soft stress-strain for stress perpendicular to order



Warner Finkelmann

Neoclassical Elastomer Theory



Warner and Terentjev

Gel: random walks between crosslinks with probability distribution

$$P(R) = \left[\frac{\det l}{(2\pi L)^3} \right]^{1/2} \exp(-3R_i l_{ij}^{-1} R_j / 2L)$$

$$\left[R_{0\alpha} R_{0\beta} \right]_{\text{av}} = \frac{1}{3} \ell_{0,\alpha\beta} L$$

$$\ell_{ij} = \ell_{||} n_i n_j + \ell_{\perp} (\delta_{ij} - n_i n_j) \quad R_i = \Lambda_{i\alpha} R_{\alpha}^0$$

$$P_0(R_0) = \left[\frac{\det l_0}{(2\pi L)^3} \right]^{1/2} \exp(-3R_{0\alpha} l_{0,\alpha\beta}^{-1} R_{0\beta} / 2L)$$

l = anisotropic step-length tensor

l_0 = tensor at time of crosslinking

$$\left[R_{0\alpha} R_{0\beta} \right]_{\text{av}} = \frac{1}{3} \ell_{0,\alpha\beta} L$$

Stretch from Step Anisotropy

Free energy density

$$\begin{aligned}
 f &= -nT[\ln P(R)]_{\text{av}} \\
 &= \frac{3}{2L} nT \Lambda_{i\alpha} l_{ik}^{-1} \Lambda_{k\beta} [R_{0\alpha} R_{0\beta}]_{\text{av}} \\
 &= \frac{1}{2} nT \text{Tr} \underline{\underline{\Lambda}} \underline{\underline{l}}_0^T \underline{\underline{\Lambda}}^{-1}
 \end{aligned}$$

Uniaxial constant volume stretch

$$\underline{\underline{\Lambda}} = \begin{pmatrix} \Lambda^{-1/2} & 0 & 0 \\ 0 & \Lambda^{-1/2} & 0 \\ 0 & 0 & \Lambda \end{pmatrix}$$

Minimize over Λ at fixed l 's

$$f = \frac{1}{2} nT [\Lambda^2 l_{0,\parallel} / l_{\parallel} + 2\Lambda^{-1} l_{0,\perp} / l_{\perp}]$$

$$\Lambda = \left(\frac{l_{0,\perp} l_{\parallel}}{l_{0,\parallel} l_{\perp}} \right)^{1/3} \rightarrow \left(\frac{l_{\parallel}}{l_{\perp}} \right)^{1/3} \quad l_{\parallel} > l_{\perp} : \Lambda > 1 \text{ as expected}$$

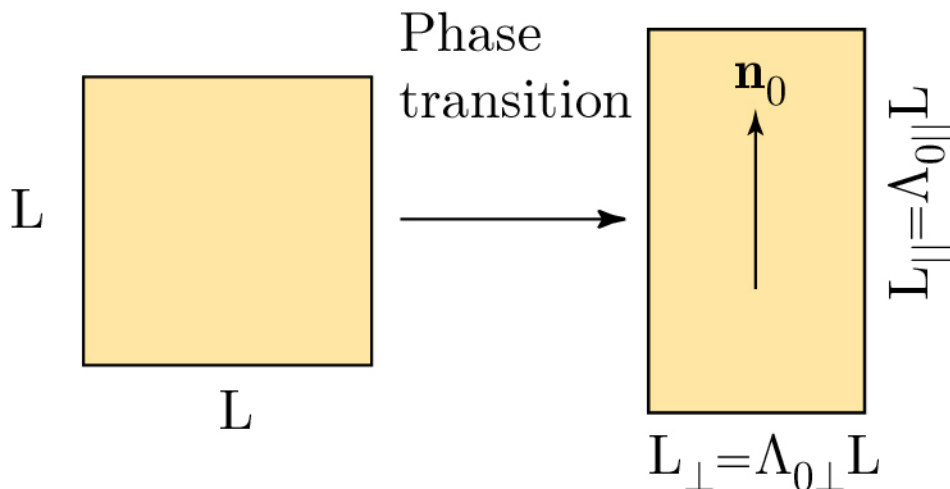
Model for Isotropic-Nematic Trans.

$$\begin{aligned}\bar{u}_{\alpha\beta} &= u_{\alpha\beta} - \frac{1}{3}\delta_{\alpha\beta}u_{\gamma\gamma} \\ &= \Psi(n_\alpha n_\beta - \frac{1}{3}\delta_{\alpha\beta})\end{aligned}$$

Deviatoric strain: like the order parameter for the isotropic-to-nematic transition

$$f = \frac{1}{2}Bu_{\alpha\alpha}^2 + \mu\text{Tr}\bar{u}^2 - C\text{Tr}\bar{u}^3 + D(\text{Tr}\bar{u}^2)^2 - Eu_{\alpha\alpha}\text{Tr}\bar{u}^2$$

μ approaches zero signals a transition to a nematic state with a nonvanishing Ψ . $u_{\alpha\alpha} \sim \Psi^2$



$$\begin{aligned}\tilde{u}_0 &= \frac{1}{2}\left(\tilde{\Lambda}_0^T \tilde{\Lambda}_0 - \underline{\delta}\right) \\ &= \bar{u}_0 + \frac{1}{3}\delta_{\alpha\alpha}u_{\alpha\alpha}\end{aligned}$$

Direction of \mathbf{n}_0 is arbitrary:
Broken continuous symmetry!

Broken Continuous Symmetry: Goldstone Modes

Goldstone Theorem: an ordered state that breaks a continuous symmetry (e.g. a rotational symmetry) necessarily has one or more zero energy modes (excitations)

\mathbf{m} : 2D magnetization; $f(\mathbf{m})$: invariant under

$$\begin{pmatrix} m_x \\ m_y \end{pmatrix} \rightarrow \begin{pmatrix} \cos \theta & -\sin \theta \\ \sin \theta & \cos \theta \end{pmatrix} \begin{pmatrix} m_x \\ m_y \end{pmatrix} \approx \begin{pmatrix} m_x - \theta m_y \\ \theta m_x + m_y \end{pmatrix}$$

$$\frac{df}{d\theta} = -\frac{\partial f}{\partial m_x} m_y + \frac{\partial f}{\partial m_y} m_x = 0$$

$$= -h_x m_y + h_y m_x = 0$$

$$\left. \frac{\partial}{\partial h_y} \frac{df}{d\theta} \right|_{m_y, h_y=0} = -h_x \frac{\partial m_y}{\partial h_y} + m_x = 0$$

$$\chi_{yy} = \frac{\partial m_y}{\partial h_y} = \frac{m_x}{h_x} \xrightarrow{h_x \rightarrow 0} \infty$$

There must be a zero mode:
It is the trivial rigid rotation
of the magnetization.

Strain of New Phase

$$\begin{aligned} R_i(\mathbf{x}) &= \Lambda_{0ij} x_j + \delta u_i(\mathbf{x}) \\ &= x'_i + u'_i(\mathbf{x}') \end{aligned}$$

$$\Lambda_{ij} = \frac{\partial R_i}{\partial x_j} = \frac{\partial R_i}{\partial x'_k} \frac{\partial x'_k}{\partial x_j} = \Lambda'_{ik} \Lambda_{0kj}$$

$$\begin{aligned} \delta \underline{u} &= \underline{u} - \underline{u}_0 \\ &= \frac{1}{2} \left(\underline{\Lambda}^T \underline{\Lambda} - \underline{\Lambda}_0^T \underline{\Lambda}_0 \right) \\ &= \underline{\Lambda}_0^T \underline{u}' \underline{\Lambda}_0 \end{aligned}$$

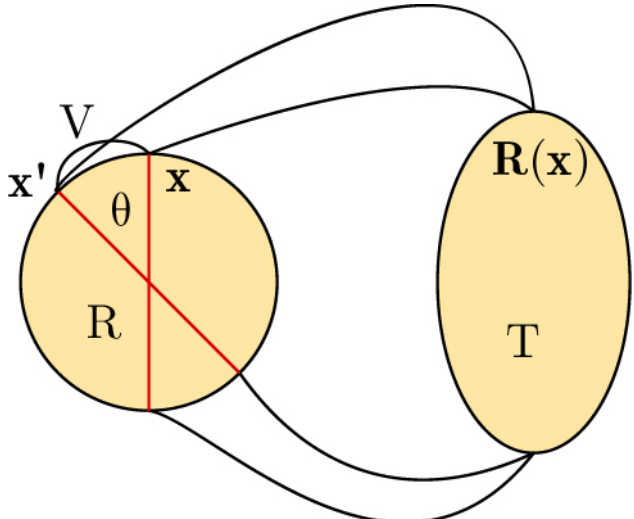
$$\underline{u}' = \frac{1}{2} \left(\underline{\Lambda}'^T \underline{\Lambda}' - \underline{\delta} \right) \approx \frac{1}{2} (\underline{\eta}' + \underline{\eta}'^T)$$

\underline{u}' is the strain relative to the new state at points \mathbf{x}'

$\delta \underline{u}$ is the deviation of the strain relative to the original reference frame R from \underline{u}_0 , and half the difference between the original metric and the new one.

$\delta \underline{u}$ is linearly proportional to \underline{u}'

Elasticity of New Phase



Rotation of anisotropy direction costs no energy

$$r = \frac{\Lambda_{0||}^2}{\Lambda_{0\perp}^2} > 1$$

$$\underline{u}' = (\underline{\Lambda}_0^T)^{-1} \left(\underline{V} \underline{u}_0 \underline{V}^{-1} - \underline{u}_0 \right) \underline{\Lambda}_0^{-1}$$

$$= \frac{1}{4} (r - 1) \begin{pmatrix} 1 - \cos 2\theta & \frac{1}{\sqrt{r}} \sin 2\theta \\ \frac{1}{\sqrt{r}} \sin 2\theta & -\frac{1}{r} (1 - \cos 2\theta) \end{pmatrix}$$

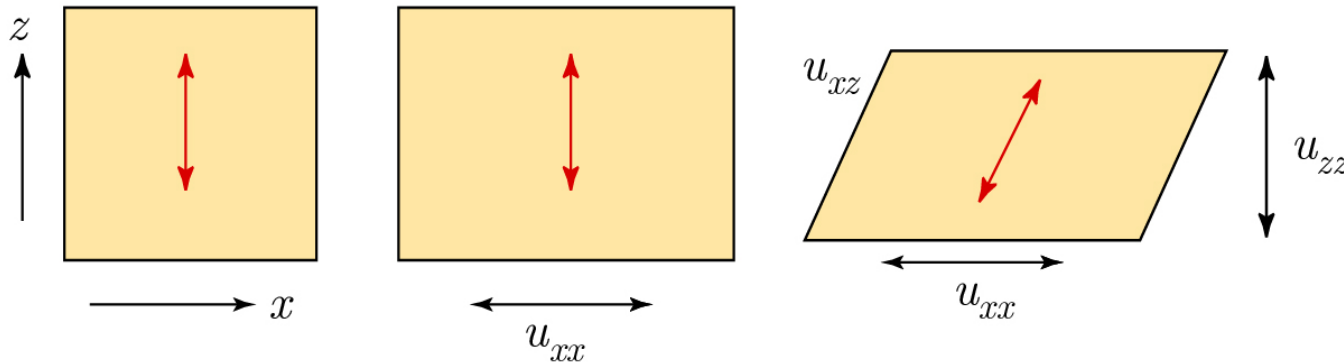
$$u'_{xz} \sim \frac{(r - 1)}{2\sqrt{r}} \theta$$

$C_5 = 0$ because of rotational invariance

$$f_{el} = \frac{1}{2} K_1 u'_{zz}{}^2 + K_2 u'_{zz} u'_{\nu\nu} + \frac{1}{2} K_3 u'_{\nu\nu} u'_{\nu\nu}$$

$$+ 2K_4 u'_{\nu\tau} u'_{\nu\tau} + \cancel{2K_5 u'_{z\nu} u'_{z\nu}}$$

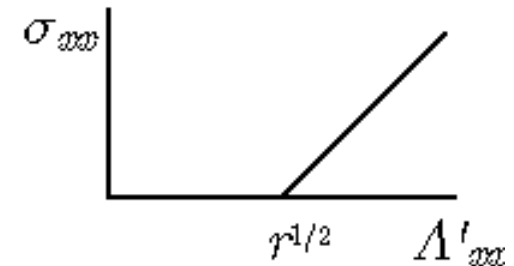
Soft Extensional Elasticity



$$\underline{u} = \frac{1}{4}(r-1) \begin{pmatrix} 1 - \cos 2\theta & \frac{1}{\sqrt{r}} \sin 2\theta \\ \frac{1}{\sqrt{r}} \sin 2\theta & -\frac{1}{r}(1 - \cos 2\theta) \end{pmatrix}$$

$$u_{zz} = -\frac{1}{r} u_{xx}$$

$$u_{xz} = \frac{1}{2\sqrt{r}} \sqrt{u_{xx}(r-1-2u_{xx})}$$



Strain u_{xx} can be converted to a zero energy rotation by developing strains u_{zz} and u_{xz} until $u_{xx} = (r-1)/2$

Frozen anisotropy: Semi-soft

System is now uniaxial – why not simply use uniaxial elastic energy? This predicts linear stress-strain curve and misses lowering of energy by reorientation:

$$f = \frac{1}{2} K_1 u_{zz}^2 + K_2 u_{zz} u_{\nu\nu} + \frac{1}{2} K_3 u_{\nu\nu}^2 + K_4 u_{\nu\tau}^2 + 2K_5 u_{\nu z}^2$$

Model Uniaxial system:

Produces harmonic uniaxial energy for small strain but has nonlinear terms – reduces to isotropic when $h=0$

$$\frac{\partial f}{\partial u_{\alpha\beta}} = \sigma_{\alpha\beta}^H = \sigma_{\alpha\beta}$$

$f(u)$: isotropic

Rotation $u \rightarrow u' = u + \theta \begin{pmatrix} -2u_{xz} & u_{xx} - u_{zz} \\ u_{xx} - u_{zz} & 2u_{xz} \end{pmatrix}$

Semi-soft stress-strain

$$\frac{df}{d\theta} = \frac{\partial f}{\partial u_{xz}} \frac{du_{xz}}{d\theta} + \frac{\partial f}{\partial u_{zx}} \frac{du_{zx}}{d\theta} + \frac{\partial f}{\partial u_{xx}} \frac{du_{xx}}{d\theta} + \frac{\partial f}{\partial u_{zz}} \frac{du_{zz}}{d\theta} = 0$$

$$\frac{df}{d\theta} = 2\sigma_{xz} (u_{xx} - u_{zz}) + 2(\sigma_{zz} - \sigma_{xx})u_{xz} = 0$$

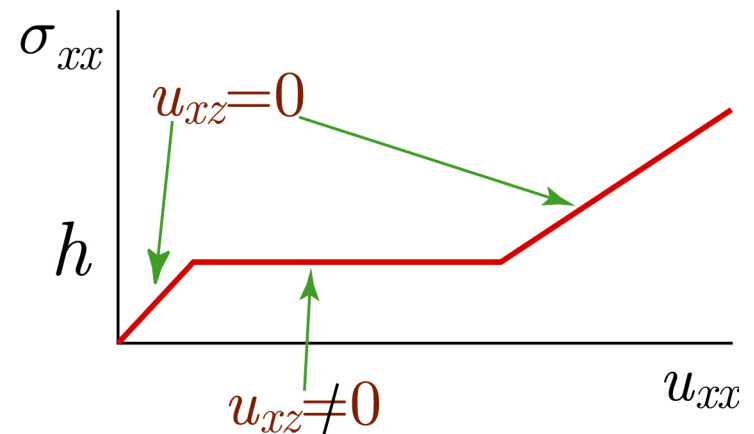
Ward Identity

$$\sigma_{xz} = \frac{(\sigma_{xx} - \sigma_{zz})u_{xz}}{u_{xx} - u_{zz}} = 0 \Rightarrow u_{xz} = 0 \text{ or } \sigma_{xx} = \sigma_{zz}$$

$$\sigma_{\alpha\beta} = \frac{\partial f}{\partial u_{\alpha\beta}}$$

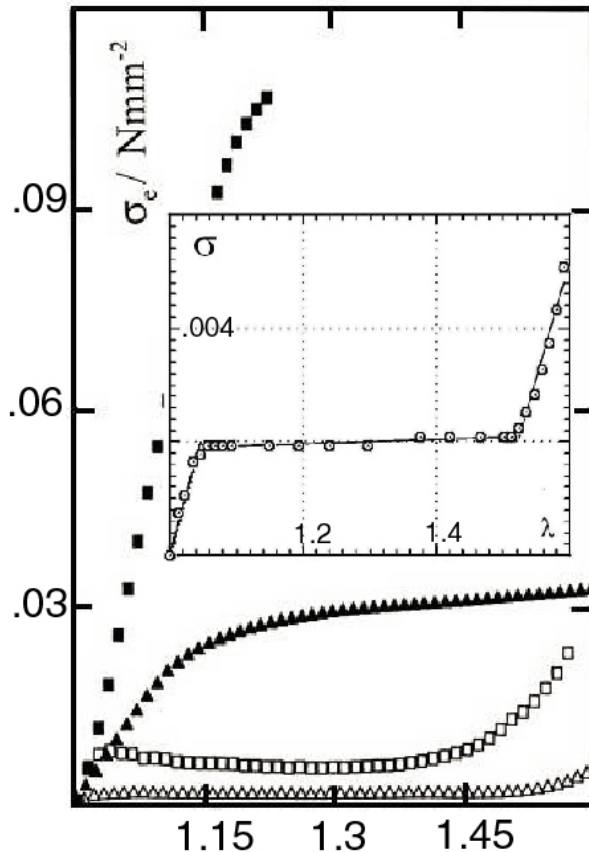
σ_{zz} : internal stress;
 σ_{xx} : 2nd PK form of external stress;
 $\sigma_{xz} = 0$.

Second PK stress tensor.

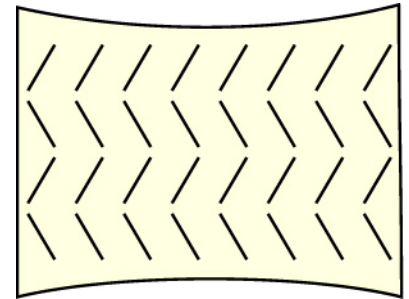


Semi-soft Extensions

Break rotational symmetry



Stripes form in real systems: semi-soft, BC



Not perfectly soft because of residual anisotropy arising from crosslinking in the the nematic phase - **semi-soft**.
length of plateau depends on magnitude of spontaneous anisotropy r .

Warner-Terentjev

Note: Semi-softness only visible in nonlinear properties

Finkelmann, et al., J. Phys. II **7**, 1059 (1997);
Warner, J. Mech. Phys. Solids **47**, 1355 (1999)

Elastic Membranes

Elastic membranes are two-dimensional manifolds that live in a three dimensional space. Thus, not only are the reference and target spaces different, they have different dimensionalities as well. It is useful to generalize this concept to D -dimensional manifolds fluctuating in a d -dimensional space

$$u_{\alpha\beta} = \left(\partial_{\alpha} u_{\beta} + \partial_{\beta} u_{\alpha} + \partial_{\alpha} \mathbf{u} \cdot \partial_{\beta} \mathbf{u} + \partial_{\alpha} \mathbf{h} \cdot \partial_{\beta} \mathbf{h} \right) \quad \text{Foppl-von Karman number}$$

$$\mathcal{H} = \frac{1}{2} \int d^D x \left[\lambda u_{\alpha\alpha}^2 + 2\mu u_{\alpha\beta} u_{\alpha\beta} + \kappa \left(\partial^2 \mathbf{h} \right)^2 \right] \quad \gamma = Y_{2D} L^2 / \kappa$$

$$S_{hh}(\mathbf{q}) = \frac{T}{\kappa q^4}; \quad S_{uu}(\mathbf{q}) \approx \frac{T}{\mu q^2} \quad \text{Harmonic order}$$

$$\langle h^2(\mathbf{x}) \rangle = \int_{L^{-1}}^{q_c} \frac{d^D q}{(2\pi)^D} \frac{T}{\kappa q^4} \approx L^{2\zeta} = L^{4-D} \quad \zeta = (4-D)/2 \text{ is the wandering exponent}$$

Nonlinearities

$$\mathcal{H}_{\text{nl}} \approx \frac{1}{2} \int d^D x \left[\lambda (\partial_\alpha u_\alpha \partial_\beta \mathbf{h} \cdot \partial_\beta \mathbf{h} + \frac{1}{4} (\partial_\beta \mathbf{h} \cdot \partial_\beta \mathbf{h})^2) + \right. \\ \left. 2\mu (\partial_\alpha u_\beta \partial_\alpha \mathbf{h} \cdot \partial_\beta \mathbf{h} + \frac{1}{4} (\partial_\alpha \mathbf{h} \cdot \partial_\beta \mathbf{h})^2) \right]$$

Integrate over \mathbf{h} (or use your favorite diagrammatic technique): Divergent contribution to μ for $D < 4$.

Expect new critical exponents

$$\mu' \approx \mu \left(1 - \frac{\mu}{T} \int d^D q q^4 S_{hh}^2(q) \right) \\ \approx \mu \left(1 - \frac{\mu T}{\kappa^2} \int_{q_L}^{q_U} \frac{q^4 d^D q}{q^8} \right) \approx \mu \left(1 - \frac{A\mu T}{(4-D)\kappa^2 q_L^{4-D}} \right)$$

$$S_{hh}(\mathbf{q}) \sim q^{-(4-\eta)}; \quad \mathbf{h}(\mathbf{q}) = \zeta_h \mathbf{h}(b\mathbf{q})$$

$$\langle \mathbf{h}(\mathbf{q}_1) \cdot \mathbf{h}(\mathbf{q}_2) \rangle = S_{hh}(\mathbf{q}_1) (2\pi)^D \delta(\mathbf{q}_1 + \mathbf{q}_2) = \zeta_h^2 \langle \mathbf{h}(b\mathbf{q}_1) \cdot \mathbf{h}(b\mathbf{q}_2) \rangle \\ = \zeta_h^2 S_{hh}(b\mathbf{q}_1) (2\pi)^D \delta(b\mathbf{q}_1 + b\mathbf{q}_2) = \zeta_h^2 b^{-D} S_{hh}(b\mathbf{q}_1) (2\pi)^D \delta(\mathbf{q}_1 + \mathbf{q}_2)$$

$$\Rightarrow S_{hh}(\mathbf{q}) = \zeta_h^2 b^{-D} S_{hh}(b\mathbf{q}) \sim \zeta_h^2 b^{-D} (bq)^{-(4-\eta)} \Rightarrow \zeta_h = b^{(D+4-\eta)/2}$$

Constraints of Rotational Invariance

$$S_{uu}(\mathbf{q}) \sim q^{-(2-\eta_u)}; \quad \mathbf{u}(\mathbf{q}) = \zeta_u \mathbf{u}(b\mathbf{q}) \Rightarrow \zeta_u = b^{(D+2+\eta_u)/2}$$

$$\mathbf{h}(\mathbf{x}) = \int \frac{d^D q}{(2\pi)^D} e^{i\mathbf{q}\cdot\mathbf{x}} \mathbf{h}(\mathbf{q}) = \int \frac{d^D q'}{(2\pi)^D} b^{-D} e^{i\mathbf{q}'\cdot(\mathbf{x}/b)} \zeta_h \mathbf{h}(\mathbf{q}') = b^{-(D-4+\eta)/2} \mathbf{h}(\mathbf{x}/b)$$

$$\mathbf{u}(\mathbf{x}) = b^{-(D-2-\eta_u)/2} \mathbf{u}(\mathbf{x}/b) \Rightarrow S_{hh}(\mathbf{x}, 0) \sim |\mathbf{x}|^{-(D-4+\eta)}; \quad S_{uu}(\mathbf{x}, 0) \sim |\mathbf{x}|^{-(D-2-\eta_u)}$$

Rotational invariance requires all terms in H scale the same way

$$\mathcal{H}_{\text{nl}} \approx \frac{1}{2} \int d^D x [2\mu(\partial_\alpha u_\beta \partial_\alpha u_\beta + \partial_\alpha u_\beta \partial_\alpha \mathbf{h} \cdot \partial_\beta \mathbf{h} + \frac{1}{4}(\partial_\alpha \mathbf{h} \cdot \partial_\beta \mathbf{h})^2 + \dots)]$$

$$(\partial u)^2 \rightarrow b^{-2} b^{-(D-2-\eta_u)} (\partial u)^2$$

$$\partial u (\partial h)^2 \rightarrow b^{-3} b^{-(D-2-\eta_u)/2} b^{-(D-4+\eta)} \partial u (\partial h)^2$$

$$(\partial h)^4 \rightarrow b^{-4} b^{-2(D-4+\eta)} (\partial h)^4$$

Equate Exponents $\eta_u + 2\eta = 4 - D$

Results

Expansion in $\varepsilon=4-D$: $\eta = \frac{12\varepsilon}{24 + d_c}; \quad \eta_u = \frac{d_c \varepsilon}{24 + d_c}; \quad d_c = d - D$

Aronowitz and TCL, PRL **60**, 2132 (1988)

Self-Consistent Field theory, $D=2, d=3$ $\eta = 0.821; \quad \eta_u = 0.358$

Le Doussal, Radzhovsky, PRL **69**, 1209 (1992)

Comments: κ stiffens and μ softens with wavenumber

$$\underline{x} = L_x \tilde{x}; \quad \underline{u} = L_u \tilde{u}; \quad h = u L_h \tilde{h}$$

$$\underline{u} \sim \partial u + (\partial h)^2 = L_x^{-1} L_u \tilde{\partial} \tilde{u} + L_x^{-2} L_h^2 (\tilde{\partial} \tilde{h})^2$$

$$\underline{u} \sim L_x^{-1} L_u \tilde{u} \text{ when } L_h^2 = L_x L_u$$

$$\kappa(q) \sim (\xi_G q)^{-\eta}$$

$$\mu(q) \sim (\xi_G q)^{\eta_u}$$

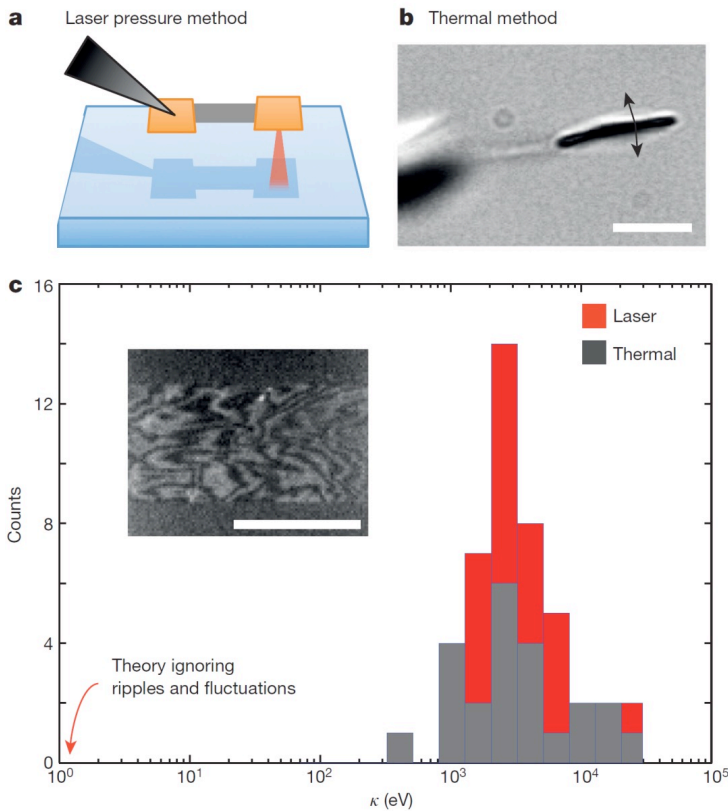
$\xi_G = \text{Ginzburg length}$

$$\int d^D x \left[\frac{\mu}{T} \underline{u}^2 + \frac{\kappa}{T} (\partial^2 h)^2 \right] = \int d^D \tilde{x} L_x^D \left[L_x^{-2} L_u^2 \frac{\mu}{T} \underline{u}^2 + L_x^{-4} L_h^2 \frac{\kappa}{T} (\partial^2 h)^2 \right]$$

Choose: $L_x^{D-2} L_u^2 \frac{\mu}{T} = L_x^{D-4} L_h^2 \frac{\kappa}{T} = 1 \Rightarrow L_x = \left(\frac{\kappa^2}{\mu T} \right)^{1/(4-D)} = \xi_G$

Experiments

Blees, ... McEuen, Nature **524**, Issue 7564,204 (2015);
 Kosmrlj and Nelson, PRB **93**, 125431 (2016);
 Wan, Bowick, Nelson, PRB **96**, 014106 (2017)



Measured κ is ~ 4000 times larger than microscopic value of $\kappa_0 = 1.2$ eV. Measurements done by direct measurements of displacement in response to force and of cantilever spring constant.

$$\frac{\kappa_{\text{eff}}}{\kappa_0} = \left(\frac{W}{\xi_G} \right)^\eta ; \quad \xi_G^2 = \frac{32\pi^2 \kappa_0^2}{3Y_{2D} k_B T}$$

$$Y_{2D} = \frac{4B\mu}{B + \mu} : \quad 2D \text{ Young's modulus}$$

Spontaneous Symmetry Breaking

Phase transition to anisotropic state as μ goes to zero

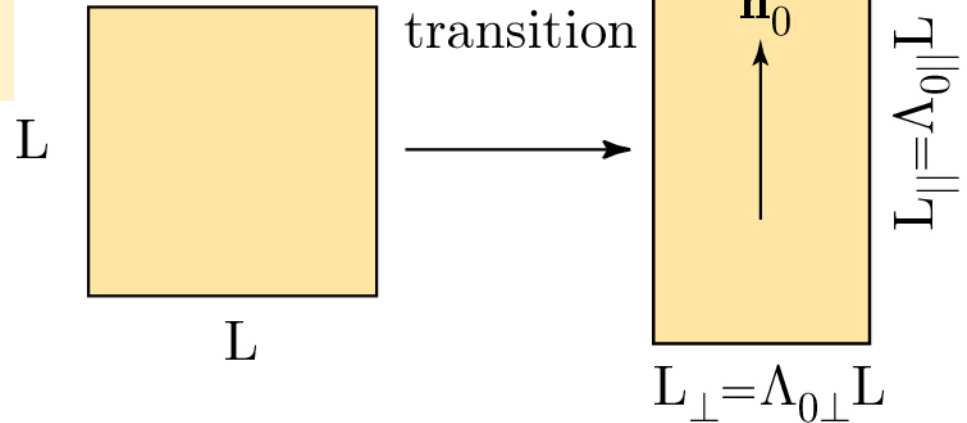
$$\underline{u}_0 = \frac{1}{2} \left(\underline{\Lambda}_0^T \underline{\Lambda}_0 - \underline{\delta} \right)$$

$$\underline{\Lambda}_0 = \sqrt{\underline{\delta} + 2\underline{u}_0}$$

$$\begin{aligned} \tilde{u}_{\alpha\beta} &= \tilde{u}_{0\alpha\beta} \\ &= \Psi \left(n_\alpha^0 n_\beta^0 - \frac{1}{3} \delta_{\alpha\beta} \right) \end{aligned}$$

Symmetric-
Traceless
part

Phase
transition



Direction of \mathbf{n}_0 is
arbitrary

$$u_{\alpha\alpha} \sim \Psi^2$$